

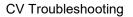
# **RediSem CV LED Driver Troubleshooting**

## Overview

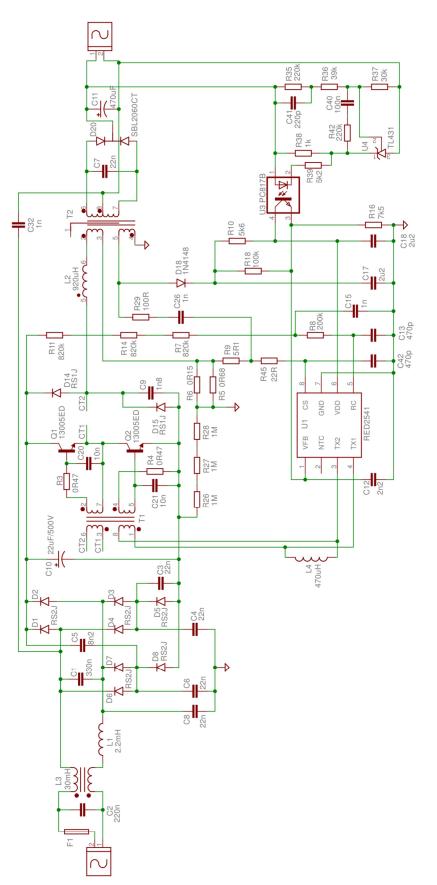
This Quick Start Guide is a companion document to AN2117, the CV LED Design Guide and is intended to help you with troubleshooting your prototype LED driver. It assumes that your prototype is based on a standard RediSem Driver Application using the RED2541 LED CV control IC and uses the same component references for quick and easy reference.

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# **Troubleshooting Steps**

**Important Note**: when attaching probes to the board under test, use a large common-mode choke in the line input to avoid getting misleading results and waveforms, and even damaging the circuit under test. It is best to use COM (pin 7 of the controller IC) as the scope ground reference point.

# Start-up Problems

### VDD rail stuck low

Check the VDD pin for a sawtooth waveform (Figure 2) – this shows that the IC (RED2541) is attempting to start up. If the VDD rail is stuck below 3.3V and there is no sawtooth, check:

D<sub>18</sub> damaged or wrong way round R<sub>18</sub> or R<sub>19</sub> value too low (remove them temporarily) R<sub>7</sub>, R<sub>8</sub>, R<sub>11</sub>, R<sub>14</sub>, R<sub>26</sub>, R<sub>27</sub>, R<sub>28</sub> values too high C<sub>13</sub>, C<sub>15</sub> or C<sub>17</sub> leaky U<sub>3</sub> (optocoupler) damaged RED2541 inserted the correct way around



Figure 2: VDD (repeated re-start attempts)

### No drive pulses

If the VDD sawtooth looks OK, next check TX1, TX2 pins on IC (RED2541) for drive pulses (Figure 3). If no pulses present, check:

 $R_{15}$ ,  $R_{41}$  open-circuit RED2541 pin 2 (NTC input) shorted to GND L<sub>4</sub> too small (remove temporarily)

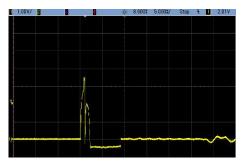


Figure 3: Tx pin drive pulse

### **BJTs not commutating**

If there are drive pulses on TX1, TX2, check the Mid-Point node (junction of  $Q_1$  emitter and  $Q_2$  collector) for commutation (use HTas the scope reference point). See Figure 4. If no commutation, possible faults include:

T<sub>1</sub> windings incorrect R<sub>3</sub>, R<sub>4</sub> damaged Q<sub>1</sub>, Q<sub>2</sub> damaged RED2541 pin 8 (CS input) open-circuit C<sub>9</sub>, C<sub>7</sub> too big Open-circuit fault in primary current loop

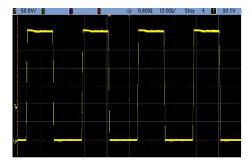


Figure 4: mid-point commutation

### No output

If the BJTs are commutating, check the output terminals for sign of short-circuit fault (disconnect line and load terminals first). A short-circuit can be caused by a faulty output diode ( $D_{20}$ ) or reversed output capacitor C<sub>11</sub>. If no short-circuit is found, check:

T<sub>2</sub> secondary windings phasing D<sub>20</sub> output diodes



# Turns on, but turns off after 1-5ms

### Foldback Protection

The RED2541 includes a foldback protection to abandon startup if an abnormal load condition is detected. In foldback, the current limit is set to 50% until the output voltage reaches 30%. It is best to configure the E-load in constant resistance (CR) mode. However, if you have to test with an E-load in Constant Current (CC) mode, you must configure it to be inactive while the output voltage is below 30%.

Normal loads must comply with the characteristics shown in Figure 5. Suitable loads include the following:

- LED, CR (constant resistance) and CV (constant voltage);
- CC (constant current) and CP (constant power) load must be inactive when VLOAD < 30% VNOM.

[Special note for CP loads and high capacitance loads: if the load requires a large current to pull it up, increase the value of R45 (maximum permitted value is  $130\Omega$ ) but beware of higher peak currents in the primary loop causing problems – inductor saturation, etc]

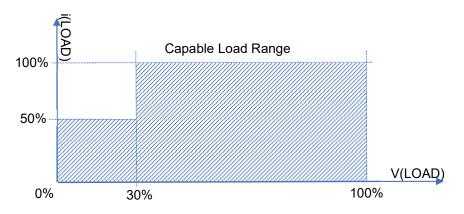


Figure 5: Static characteristics of allowed loads

### VDD Supply drops out

Check VDD and primary current during start up (Figure 6). If VDD drops below 2.4V during the start-up, the IC will stop and re-start. Possible causes are:

C<sub>18</sub> too small C<sub>11</sub> (or load capacitance) too large Current Limit too low T<sub>2</sub> aux winding too few turns R<sub>10</sub> value too large D<sub>18</sub> faulty/missing R<sub>18</sub> value incorrect Secondary regulation error R<sub>16</sub>, R<sub>41</sub> missing C<sub>12</sub> s/c fault

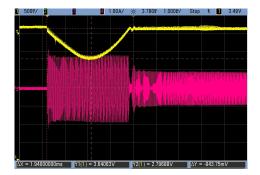


Figure 6: VDD, primary current (good startup)

If the load requires a large current to pull it up, increase the value of R45 (maximum permitted value is  $130\Omega$ ) but beware of higher peak currents in the primary loop causing problems – inductor saturation etc.



### **VFB Low Fault**

If VDD looks OK during startup, check RED2541 pin 1 (VFB input) during startup (Figure 7). If the VFB pin voltage has not risen above 300mV after 128 cycles (about 3ms), the controller registers a fault, shuts down and attempts to re-start. If this occurs, check:

 $\begin{array}{l} R_{18} \mbox{ missing or incorrect size} \\ R_{41} \mbox{ missing} \\ T_2 \mbox{ aux winding too few turns} \end{array}$ 

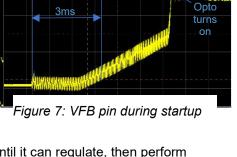
# **Full load Regulation Problems**

If the converter cannot maintain the output at full load, reduce the load until it can regulate, then perform the following checks:

### **Oscillator error**

Monitor RED2541 pin 5 (RC input) waveform (Figure 8) through a line cycle. Check that the highest waveform peaks are less than 2.2V at full load. If not, check:

C<sub>42</sub> value R<sub>7</sub>, R<sub>8</sub>, R<sub>11</sub>, R<sub>14</sub> values



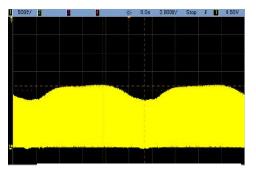


Figure 8: RC pin at full load

### **Current sensing error**

Check:

Value of  $R_5$ ,  $R_6$  (current sense resistors) Values of  $C_7$ ,  $C_{26}$ ,  $R_9$  (parallel current compensation) Phase of Aux winding on T2 – change the direction if in doubt

#### **Base Drive error**

If the inductance seen across the control winding of T1 is too small, this will limit the frequency range, reducing the maximum output power.

Check:

 $T_1,\,L_4$  inductance values (remove L4 briefly to check)  $T_1$  turns ratio



### Capacitive mode protection error

Monitor the waveforms of primary current and RED2541 pin 5 (RC), checking for capacitive mode limiting. A good design should hit the capacitive limit at full load when line input is <198Vac. (Figure 10, Figure 9).

If capacitive mode limiting occurs within the target line/load range, check:

> T₂ transformer turns ratio R₅ value Boost capacitor values

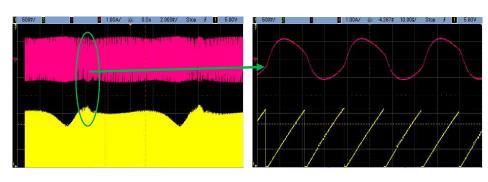


Figure 10: Primary current and RC pin on edge of capacitive mode switching

Figure 9: Primary current and RC pin on edge of capacitive mode switching (zoomed in)

### Secondary voltage regulation error

If the output appears to be regulating too low, temporarily short out  $U_3$  pins 1,2 (optocoupler inputs). If the output rises, it shows the problem is in the secondary voltage sensing circuit. Check:

R<sub>35</sub>, R<sub>36</sub>, R<sub>37</sub> values R<sub>38</sub> value too high

### **High Output Ripple**

Check the feedback loop values are all correct or similar to the suggested values. Check that there are no primary side regulation errors by increasing the value of R18. High leakage in the transformer can cause high spikes on the aux winding of T2. This is especially worse on low voltage high current designs

### Primary voltage limiting error

Run the driver with nominal line, full load and temporarily short out the optocoupler LED (U<sub>3</sub> pins 1,2). The output voltage should rise to 105-110% of the nominal output voltage. If not, adjust the value of  $R_{18}$  (decrease R18 to decrease output voltage). Other things to check:

Noise on VFB pin (because C<sub>12</sub> missing or too small)

 $T_2-aux \ winding \ - \ too \ many \ turns?$ 

T<sub>2</sub> leakage inductance – aux winding should be outermost (ie on top of the secondary windings)

## Instability

### Unstable at normal loads

Check primary current waveform for signs of instability across full range of line inputs, and load range 10%-100%. If system is unstable at nominal line voltage check:

 $C_{40}$  (increase value for more stability)  $C_{11}$ ,  $R_{35}$  (time constant should be ~50usec)  $C_{12}$ ,  $R_{41}$  (time constant should be ~20usec)  $R_{39}$  (increase value for more stability)  $R_{42}$  (too large?)  $U_3$  (optocoupler) gain factor



The values given in the reference design assume a typical low-cost optocoupler (e.g. PC817 grade B), with CTR < 260%. If the maximum CTR > 260%, consider increasing R39 value for stability. Decrease R39 for higher loop gain, lower output ripple.

If system is unstable only at low line voltage, check:

- T<sub>2</sub> turns ratio
- T1 turns ratio
- T<sub>1</sub>, L<sub>4</sub> inductance values (remove L<sub>4</sub> briefly to check)

### Unstable at low loads

Burst threshold may be too high, refer to "Burst threshold problems" section below.

### Unstable in standby

Check output voltage waveform for signs of instability in standby by stepping load from 10% and 0%. Some overshoot and undershoot is acceptable, see Figure 11. But, if instability is present, check:

C<sub>40</sub> value (too small?) C<sub>17</sub> value (too small?) R<sub>10</sub> value (too large?) R<sub>38</sub> value (too large?)



Figure 11: output voltage with load steps 0-10%

## **Burst threshold problems**

The burst threshold should normally be in the load range 5-10%.

### Burst threshold too high

If bursting occurs with loads > 10%, increase the load until it does run continuously then perform the following checks.

#### **Oscillator error**

Monitor RED2541 pin 5 (RC) waveform (Figure 12) through a line cycle. The controller IC will enter burst mode if the maximum frequency limit is reached, i.e. when the peaks of the RC waveform are <350mV.

Check that the lowest waveform peaks are >400mV. If not, check (decrease):

C<sub>42</sub> value R<sub>7</sub>, R<sub>8</sub>, R<sub>11</sub>, R<sub>14</sub> values

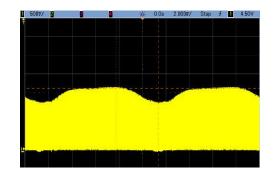


Figure 12: RC pin at 10% load



#### Load current correction error

Connect a scope probe (as close as possible) to RED2541 pin 8 (CS) and compare the waveform to the yellow trace in Figure 13 (some ringing is acceptable). If the flat parts of the waveform are very different to those shown, check:

R<sub>9</sub>, R<sub>29</sub> values C<sub>7</sub>, C<sub>26</sub> values T<sub>2</sub> construction - aux winding reversed or incorrect turns?



Figure 13: Primary current and CS pin waveforms

If the ringing is severe, check:

 $T_2$  construction details – aux winding should be on outside of secondary windings

 $T_2$  construction details – secondary windings leadouts must be short

### Burst threshold too low

In no-load condition, if the driver does not enter burst mode, there is a problem with the load current correction - see section above.

# **Hot Transistors**

### **Conduction Losses**

Using a voltage-clamped scope probe amplifier (or equivalent) measure the on-state voltage. Check that the on-state voltage of both transistors is <300mV. If the on-state is higher than this, possible causes include:

 $Q_1$ ,  $Q_2$  current rating or  $h_{FE}$  too small Base drive transformer  $T_1$  turns ratio too large

### Switching Losses

Check the storage and fall times of both transistors using scope probes to monitor the base-emitter and collector-emitter waveforms. At minimum line voltage and maximum load, the storage time ( $t_s$ ) should be roughly 200ns and the fall time ( $t_F$ ) should be <200ns. If this is not the case, possible causes include:

 $\begin{array}{l} Q_1, \, Q_2 \mbox{ too slow} \\ R_3, \, R_4 \mbox{ values too small} \\ T_1 \mbox{ inductance too high} \\ C_9 \mbox{ too small} \end{array}$ 

### Shoot-through

Monitor the collector current of  $Q_1$  (or  $Q_2$ ) using a current transformer. If there are any sharp current spikes in the waveform, please check:

Base Drive transformer  $T_1$  construction – windings bunched incorrectly Flywheel diodes  $D_{14}$ ,  $D_{15}$  turn-on too slow  $C_9$  wrong side of  $T_1$  primary winding

The ceramic capacitors  $C_{20}$ ,  $C_{21}$  between base and emitter of  $Q_1$  and  $Q_2$  help to suppress shoot-through.



## EMI

### **Conducted Emissions**

#### 50k – 500kHz

<u>Differential-mode:</u> Increase C<sub>1</sub>, C<sub>2</sub> and L<sub>1</sub> (Note: increasing C<sub>1</sub>, C<sub>2</sub> will reduce PF)

Common-mode:

Make sure that the transformer construction (order and phasing of windings) is correct. A screen winding should not be necessary, but can help if all else fails.

Minimise lengths of secondary winding leadouts.

Increase common-mode choke  $L_3$  or the Y-Capacitor  $C_{32}$ .

Check PCB tracking. Make sure that the noisy midpoint node is not close to the secondary or mains input.

#### 2MHz – 30MHz

Minimise lengths of PCB tracks associated with base drive transformer  $T_1$ .

### **Radiated Emissions**

#### 30 - 100MHz

Minimise the tracking around the T<sub>1</sub> base drive transformer. Test to see if one of the diodes  $D_{14}$ ,  $D_{15}$  is causing ringing. Add 10R in series with aux diode  $D_{18}$ . Divide the midpoint capacitor C<sub>9</sub> into two and place directly across the freewheel diodes  $D_{14}$  and  $D_{15}$ 

# **Harmonics Emissions**

### Non-compliant at low line, high load

### Boost voltage too high

 $C_3$ ,  $C_5$  values too small  $C_4$ ,  $C_6$ ,  $C_8$  values too large

### Non-compliant at high line, low load

#### Boost voltage too low

 $C_3$ ,  $C_5$  values too large  $C_1$ ,  $C_4$ ,  $C_6$ ,  $C_8$  values too small

## **Power Factor**

As for Harmonics Emissions above, plus:

C1, C2 values too large – Increase the size of the Inductor to maintain EMI compliance

# **Fault Protection**

### Short-circuit load – Bulk Supply Voltage too high (PPFC apps only)

 $T_2$  aux winding turns ratio  $T_2$  construction – Aux winding should be outside the secondary windings

### Optocoupler fault - output voltage too high

 $R_{18}$  too large Voltage control loop unstable (see above)  $C_9$  too large



 $T_1 \mbox{ or } L_4 \mbox{ inductance too large}$ 

### Capacitive Mode happens at normal line voltages

T<sub>2</sub> turns ratio too low C<sub>9</sub> value too large

### **Fault Recovery Time**

#### Too short:

 $\begin{array}{l} \mbox{Increase $C_{17}$, $C_{18}$} \\ \mbox{Increase $R_7$, $R_{11}$, $R_{14}$} \\ \mbox{(adjust $C_{13}$ to keep same clock setting)} \\ \mbox{(adjust $R_{19}$ to keep same minimum line voltage for startup)} \end{array}$ 

#### Too long:

Decrease  $C_{17}$ ,  $C_{18}$ Decrease  $R_7$ ,  $R_{11}$ ,  $R_{14}$ (adjust  $C_{13}$  to keep same clock setting) (adjust  $R_{19}$  to keep same minimum line voltage for startup)



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RediSem designs and supplies semiconductor ICs for energy efficient power management applications. RediSem uniquely combines extensive experience in power electronics with in-depth knowledge of IC design and manufacturing and works with the world's top suppliers and customers. RediSem's unique patented IC and converter technologies deliver maximum efficiency and performance, while reducing overall bill of materials cost through the use of bipolar transistors.

RediSem's range of LED control ICs can be used with RediSem's patented single stage LED control solution to provide very high efficiencies with low EMI – all with a single IC. When combined, these features deliver a low cost, high performance LED driver solution.

RediSem's fluorescent driver controller ICs achieve the advanced performance of MOSFET drivers by using bipolar transistors at a fraction of the BOM cost. RediSem's range of SMPS (Switched Mode Power Supply) control ICs enables low-cost LLC converters with bipolar transistors that deliver very high efficiencies already meeting DoE Level VI regulations, have low standby power and have much lower EMI compared to flyback converters.

All RediSem ICs are supported by comprehensive turn-key application designs enabling rapid time to market. For further information please use our contact details below

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